

# RADAR WORKSHOP

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# RADAR WORKSHOP

## Introduction to Radars

- Topics

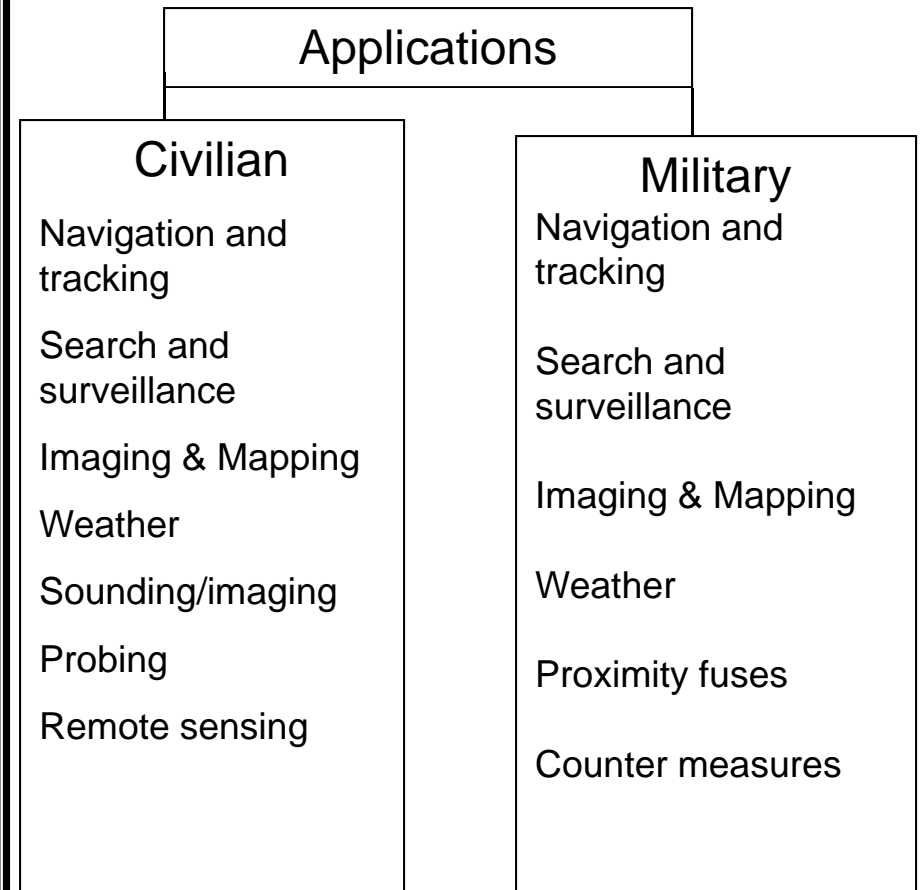
- EM Spectrum
- Plane Waves
  - Attenuation Characteristics
- Radar Equation
  - Point target
  - Plane Reflector
  - Distributed target

- Examples

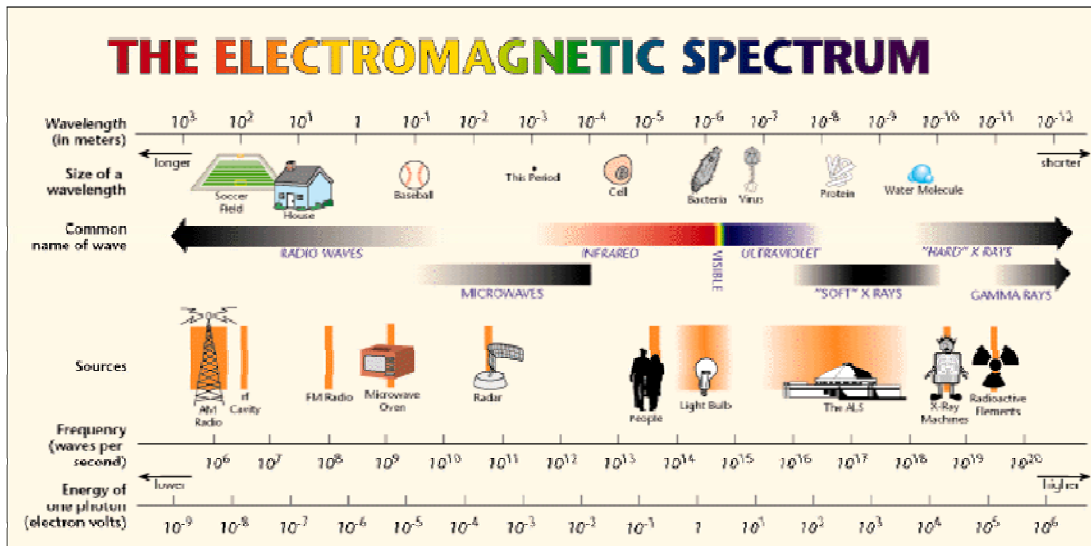
- Pulse compression
  - Principle
  - Range sidelobes
    - Solutions
- SAR
  - Principle
  - Range equation

# Radars

- Radar
  - Radio Detection and Ranging.
  - Texts:
    - Stimson, G. W., "Introduction to Airborne Radar", SciTech Publishing, 1998.
    - Skolnik, M. I., "Introduction to Radar Systems", McGraw Hill, 1981.



# EM Spectrum



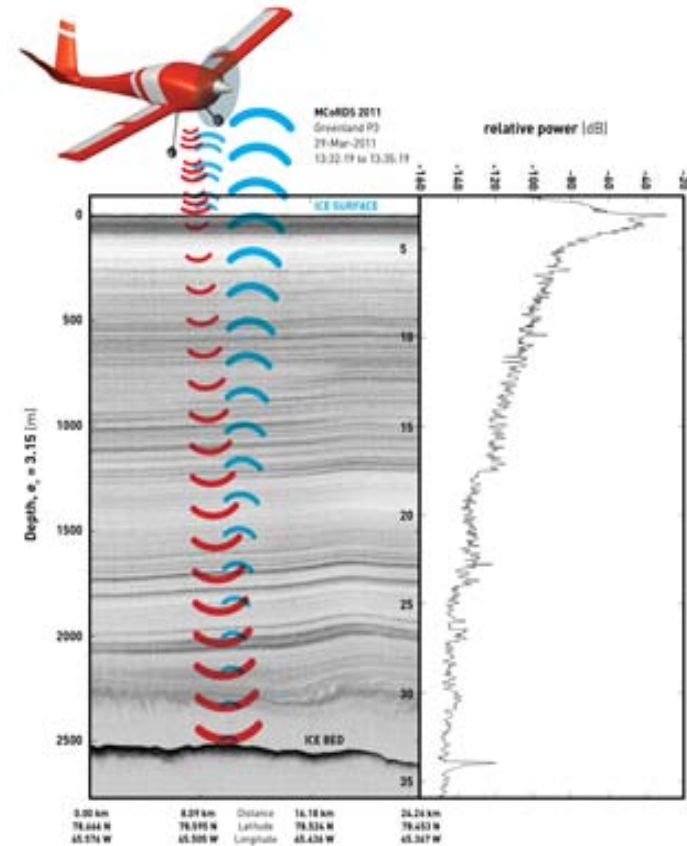
<http://www.lbl.gov/MicroWorlds/ALSTool/EMSpec/EMSpec2.html>

## Sounders/imagers

- 1-1000 MHz
  - Temperate ice
    - LF and HF
  - Ice sheets
    - HF, VHF and UHF
- Microwave region
  - 300 MHz - 30 GHz
    - Internal layers
    - Snow cover sea ice.
- Millimeter wave
  - 30 GHz - 300 GHz.
  - Internal layers
- IEEE uses a different definition
  - 300 MHz - 100 GHz

# Radars for Glaciological Applications

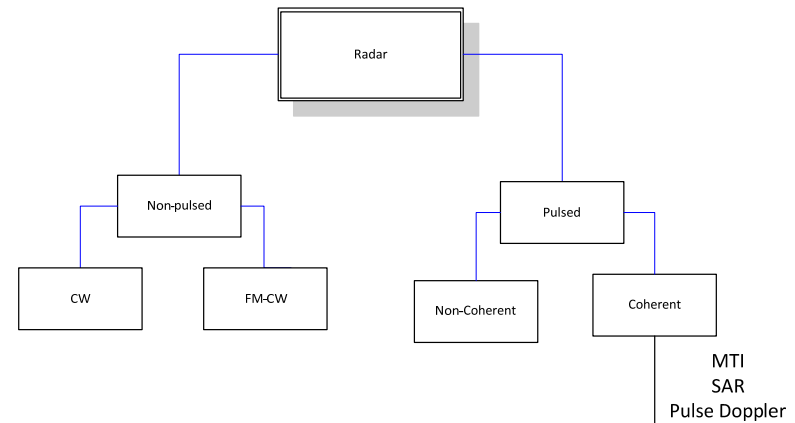
- An essential tool in glaciology
  - Ice thickness
  - Internal layers
  - Structure
  - Surface roughness
  - Bed conditions
  - 3-D topography
- Advantages
  - Wide-area coverage
    - Airborne platforms
  - Established
- Disadvantages
  - Data are difficult to interpret
  - Coarse resolution except for SAR]
- Pulse radar
- Impulse radars
- FM-CW radars
  - Step-frequency radars



CReSIS and CiC

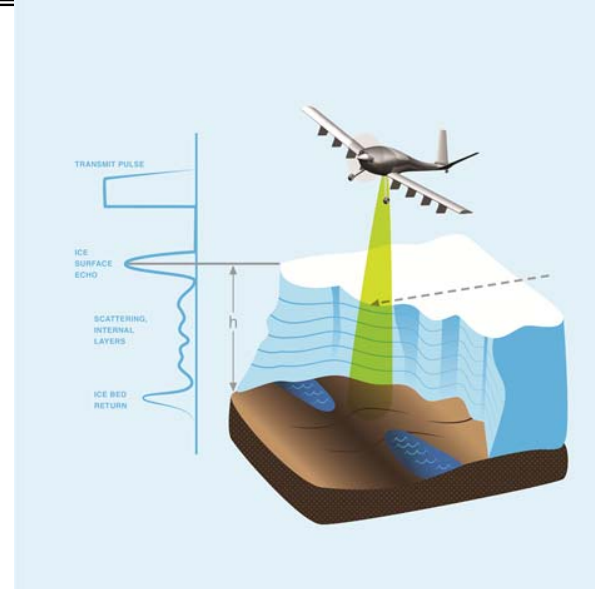
# Radar Principles

- Radar classified according to the transmit waveform.
  - Continuous
    - Doppler
    - Altimeter
    - Scatterometer
  - Pulse
    - Wide range of applications
    - Sounders/imagers
  - Impulse radar
    - LF and HF
      - Temperate ice



# Radar Principle

- Radar measures distance by measuring time delay between the transmit and received pulse.
- Measured time delay is converted to ice thickness.
- In freespace
  - 1 us = 150 m
  - 1 ns = 15 cm



$$\partial t = \tau_2 - \tau_1 = \frac{2R_2}{c} - \frac{2R_1}{c}$$

$$h = \partial t v_p$$

where  $v_p$  = velocity of propagation in ice.

# EM Theory

- Consider a plane wave in a dielectric

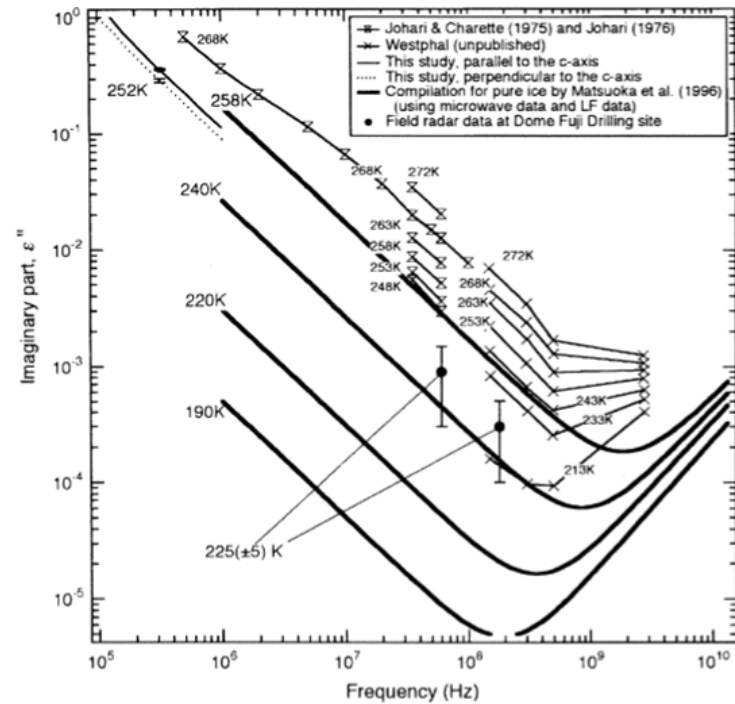
- $E(z) = E_0 e^{-\gamma z}$

$$\gamma = \alpha + j\beta = j\omega\sqrt{\mu\epsilon} = j\omega\sqrt{\mu_0\epsilon'}\left(1 - j\frac{\epsilon''}{\epsilon'}\right)$$

$$\approx j\omega\sqrt{\mu_0\epsilon'}\left(1 - j\frac{\epsilon''}{2\epsilon'}\right)$$

$$\beta \approx \omega\sqrt{\mu_0\epsilon'}$$

$$\alpha \approx \omega\sqrt{\mu_0\epsilon'}\frac{\epsilon''}{2\epsilon'} = \frac{\pi}{\lambda}\frac{\epsilon''}{\sqrt{\epsilon'}}$$

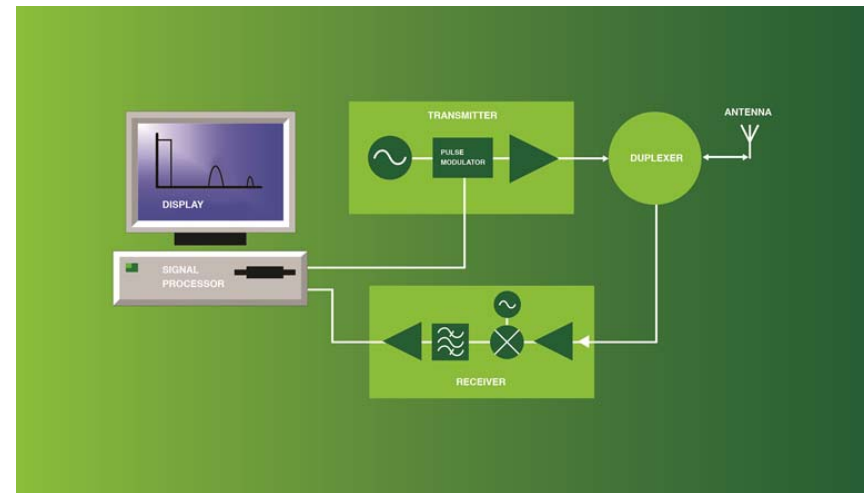


Imaginary part of the dielectric constant adapted from Fujita et al., [ 2000 ]

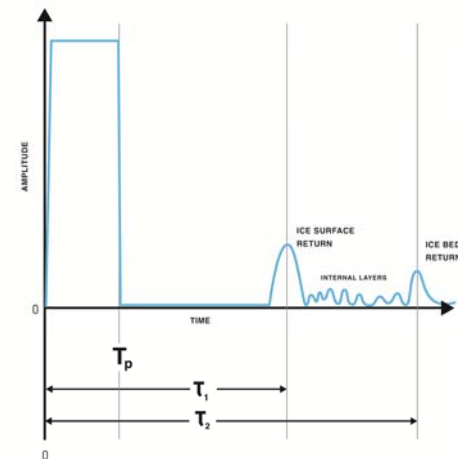


# Radar

- Block diagram of a simple pulse radar
  - It consists of a transmitter to generate a pulse-modulated carrier signal.
  - A receiver to amplify and filter the received signal.
  - A Duplexer that enables same antenna to be used for transmission and reception.
  - Signal processor.
  - Display unit - PPI, B-scope etc.

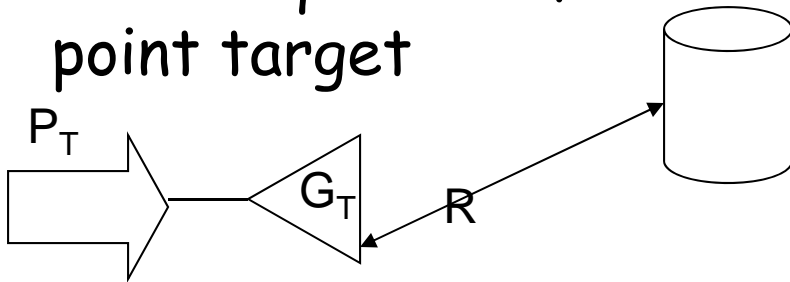


RADAR TIMING DIAGRAM



# Radar—Principle

- Radar equation of a point target



Power density at the target is given by

$$P_d = \frac{P_T G_T}{4\pi R^2}$$

Target with radar cross section,  $\sigma$ , intercepts a part of this signal and reradiates in the direction of the radar.

$$P_{dr} = \frac{P_T G_T}{4\pi R^2} \sigma$$

Reradiated power incident on the antenna is given by

$$P_{ri} = \frac{P_T G_T}{4\pi R^2} \sigma \frac{1}{4\pi R^2}$$

The receive antenna with an effective aperture,  $A_e$ , incident signal and it is given by

$$P_r = \frac{P_T G_T}{4\pi R^2} \sigma \frac{A_e}{4\pi R^2}$$

$$P_r = \frac{P_T G_T G_R \lambda^2 \sigma}{(4\pi)^3 R^4}$$

$$\text{where } G_R = \frac{4\pi A_e}{\lambda^2}$$

- For a monostatic radar
- $G_T = G_R$
- Radar sensitivity is determined by the minimum detectable signal set by the receiver noise.
- $N_o = kTBF$
- $F =$  noise figure,  $T =$  temperature
- Signal-to-noise ratio

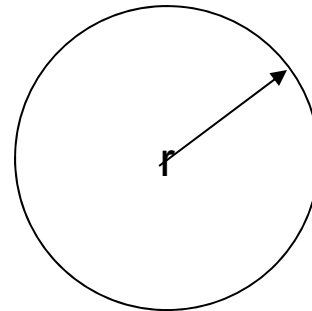
$$\frac{S}{N} = \frac{P_r}{N_o} = \frac{P_T G_T^2 \lambda^2 \sigma}{(4\pi)^3 R^4 K T B F} = \frac{[P_T A_e] G_T \sigma}{(4\pi) R^4 K T B F}$$

$$R_{\max} = \sqrt[4]{\frac{P_T G_T^2 \lambda^2 \sigma}{(4\pi)^3 \frac{S}{N} K T B F}} \sqrt[4]{\frac{[P_T \tau] G_T^2 \lambda^2 \sigma}{(4\pi)^3 \frac{S}{N} K T F}}$$

# Radar Cross-Section

- Radar cross section characterizes the size of the object as seen by the radar.
- Where?  
 $E_s$  = scattering field  
 $E_i$  = incident field

$$\sigma = \lim_{R \rightarrow \infty} 4\pi R^2 \frac{|E_s|^2}{|E_i|^2}$$



$$\sigma = \pi r^2$$

# Planar Reflector

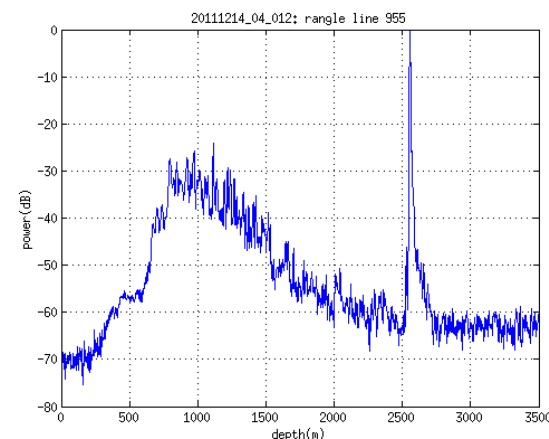
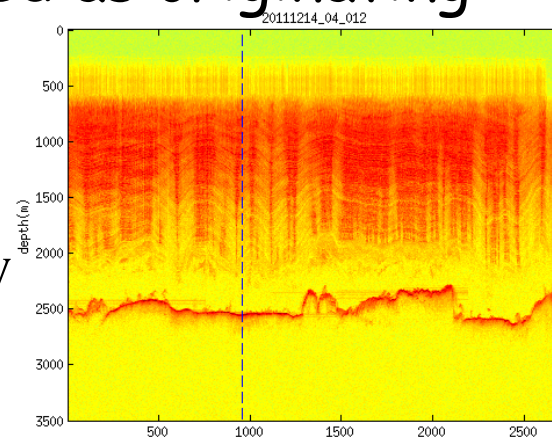
- Coherent reflections can be treated as originating from a planar reflector.

Power received from a planar reflector given by

$$P_r = \frac{P_T G_T A_e}{4\pi(2R)^2} |\Gamma|^2, \text{ where } G_R = \frac{4\pi A_e}{\lambda^2}$$

$$P_r = \frac{P_T G_T G_R \lambda^2 |\Gamma|^2}{(4\pi)^2 R^2}$$

For ice, we must add additional terms as



# Radar Equation

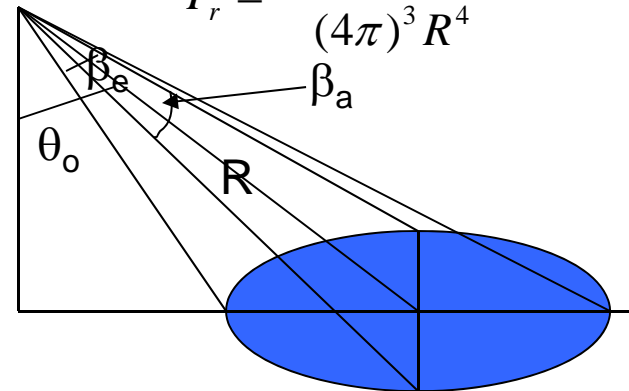
- A distributed target contains many scattering centers within the illuminated area.
- It is characterized by radar cross section per unit area, which is referred to as scattering coefficient.

$$\sigma = \sigma^0 A$$

$\sigma^0 =$  scattering coefficient

$A =$  Illuminated area

$$P_r = \frac{P_T G_T^2 \lambda^2 \sigma^0 A}{(4\pi)^3 R^4}$$



$$A = \frac{\pi}{2} R \cos(\theta_0) \left( \tan\left(\theta_0 + \frac{\beta_e}{2}\right) - \tan\left(\theta_0 - \frac{\beta_e}{2}\right) \right) R \tan\left(\frac{\beta_a}{2}\right)$$

If  $\theta_0 \ll 1$  &  $\beta \ll 1$

$$A \approx \frac{\pi}{4} R^2 \beta_e \beta_a$$

# Radar Equation

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$$P_r = \frac{P_T G_T^2 \lambda^2 \sigma^0}{(4\pi)^3 R^4} \frac{\pi R \beta_e R \beta_a}{4}$$

$$P_r = \frac{P_T G_T^2 \lambda^2 \sigma^0}{(4\pi)^2 R^2} \frac{\beta_e \beta_a}{16}$$

For a distributed target and coherent reflector, power received falls off as  $1/R^2$

For a point target power received falls off as  $1/R^4$

For a distributed target with SAR processing power can fall-off as  $1/R^{2.5}$  or  $1/R^3$

# Radar Equations for Ice

## • Planar Reflector

$$P_r = \frac{P_T G_T A_e (1 - |\Gamma_{as}|^2) |\Gamma_b|^2}{4\pi(2h)^2 L_{is}}$$

$$\left(\frac{S}{N}\right)_1 = \frac{P_r}{P_n} = \frac{P_T G_T A_e (1 - |\Gamma_{as}|^2) |\Gamma_b|^2}{4\pi(2h)^2 L_{is} k T B F}$$

For a coherent radar with pulse compression

$$\left(\frac{S}{N}\right)_M = \frac{P_T G_T A_e (1 - |\Gamma_{as}|^2) |\Gamma_b|^2 C_g M}{4\pi(2h)^2 L_{is} k T B F}$$

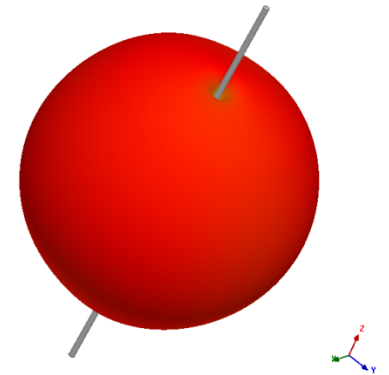
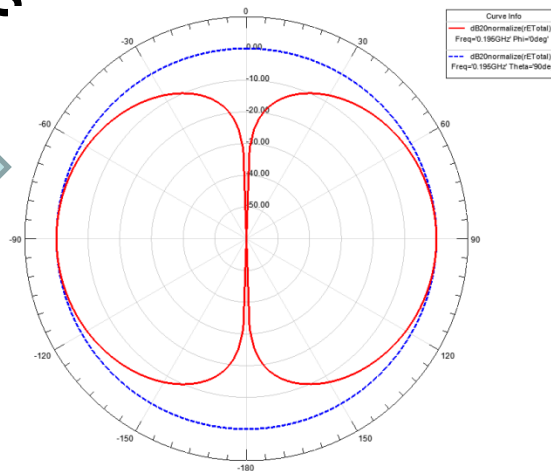
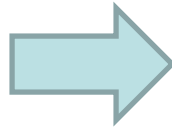
## • Distributed target with SAR processing

$$\frac{S}{N_M} = \frac{P_r}{P_n} = \frac{P_T G_T A_e \sigma^0 \pi h \beta_e \sqrt{c \tau_{pc} h \tau_{pu} M}}{2(4\pi)^2 h^4 L_{is} k T F}$$

$$\frac{S}{N_M} = \frac{P_r}{P_n} = \frac{M P_T G_T A_e \sigma^0 \beta_e \sqrt{c \tau_{pc} \tau_{pu}}}{32\pi h^{2.5} L_{is} k T F}$$

# Antennas

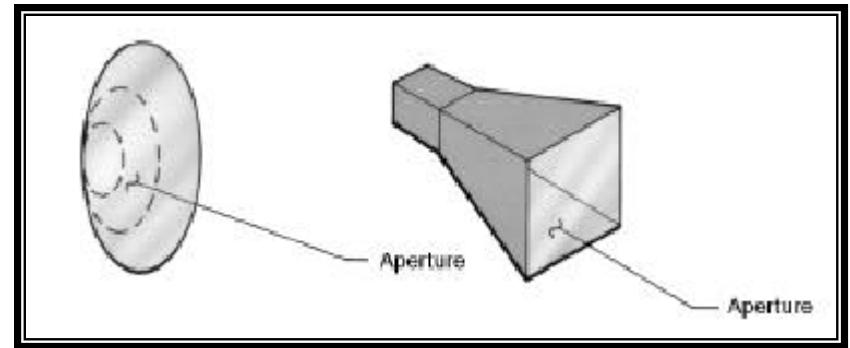
- Antennas are used to couple electromagnetic waves into free space or capture electromagnetic waves from free space.
- Type of antennas
  - Wire
    - Dipole
    - Loop antenna
  - Aperture
    - Parabolic dish
    - Horn










# Antennas

- Antennas are characterized by their:
  - Directivity
    - It is the ratio of maximum radiated power to that radiated by an isotropic antenna.
  - Efficiency
    - Efficiency defines how much of the power is the total power radiated by the antenna to that delivered to the antenna.
  - Gain
    - It is the product of efficiency and directivity
  - Beamwidth
    - Width of the main lobe at 3-dB points.

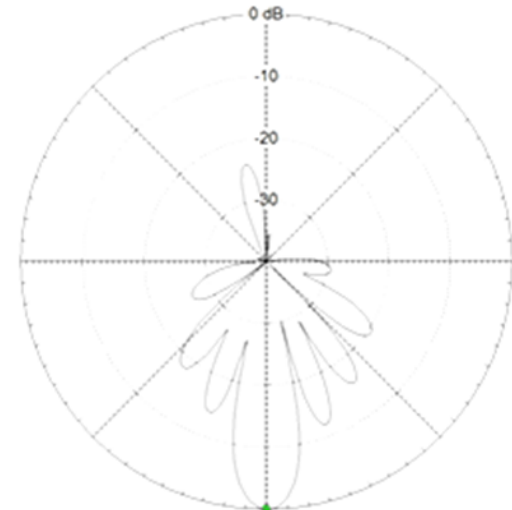


# Antenna gain

| Aperture-Type   | Beamwidth<br>(From Aperture)   | Directive gain<br>(From Aperture)                                      | Directive gain<br>(From Beamwidth)                                | Antenna Efficiency<br>(Aperture Illumination<br>Efficiency) |
|---|--|--|---|---|
| Uniformly illuminated<br>circular aperture-<br>hypothetical parabola<br><br>18 dB side-lobe level  | $\theta = \frac{58\lambda}{a}$<br>$\theta = \theta_1 = \theta_2$   | $g_d = \frac{15 a^2}{\lambda^2}$<br>$g_d = \frac{9.87 a^2}{\lambda^2}$ | $g_d = \frac{52,525}{\theta^2}$<br>$\theta = \theta_1 = \theta_2$ | 100%  |
| Uniformly illuminated<br>rectangular aperture or<br>linear array<br><br>13 dB side-lobe level  | $\theta_1 = \frac{51\lambda}{a}$<br>$\theta_2 = \frac{51\lambda}{b}$   | $g_d = \frac{1.6 a b}{\lambda^2}$                                      | $g_d = \frac{41,253}{\theta_1 \theta_2}$                          | 100%  |
| Rectangular horn<br>a) Polarization plane:<br>E-plane<br><br>13 dB side-lobe level<br>b) Orthogonal polarization<br>plane: H-plane<br><br>26 dB side-lobe level | $\theta_1 = \frac{56\lambda}{a_E}$<br><hr style="border-top: 1px dashed black;"/> $\theta_2 = \frac{67\lambda}{a_H}$ | $g_d = \frac{7.5 a_E a_H}{\lambda^2}$                                  | $g_d = \frac{31,000}{\theta_1 \theta_2}$                          | 60%   |
| Nonuniformly illuminated<br>circular aperture (10 dB<br>taper)-normal parabola<br><br>26 dB side-lobe level  | $\theta = \frac{72\lambda}{a}$<br>$\theta = \theta_1 = \theta_2$   | $g_d = \frac{5 a^2}{\lambda^2}$  | $g_d = \frac{27,000}{\theta^2}$<br>$\theta = \theta_1 = \theta_2$ | 50%   |
| $a \gg \lambda$   |  | $G_d = 10 \log_{10} g_d$ dB  | $G_d = 10 \log_{10} g_d$ dB                                       |   |

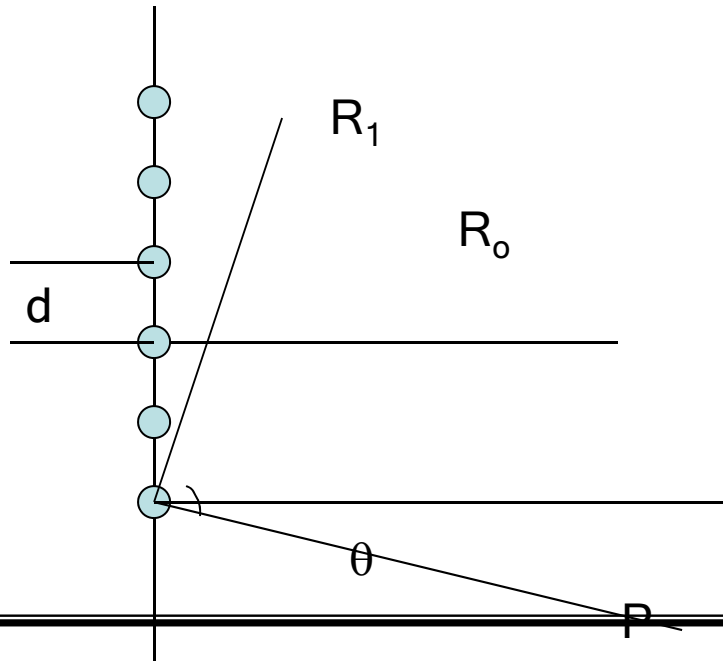
# Antennas

- An array of antennas is used whenever higher directivity is needed.
- Directivity is related to number of elements.
- Can be used for electronic scanning.
  - Most of the SAR antennas are arrays.



# Antenna Array

- Let us consider simple array consisting of isotropic radiators.



$$R_1 = R_o + d \sin(\theta)$$

$$\partial R = d \sin(\theta)$$

$$\partial \varphi = \frac{2\pi}{\lambda} d \sin(\theta)$$

$$E_i = E_o \left( e^{-j\frac{2\pi R_o}{\lambda}} + e^{-j\frac{2\pi(R_o + d \sin(\theta))}{\lambda}} \right)$$

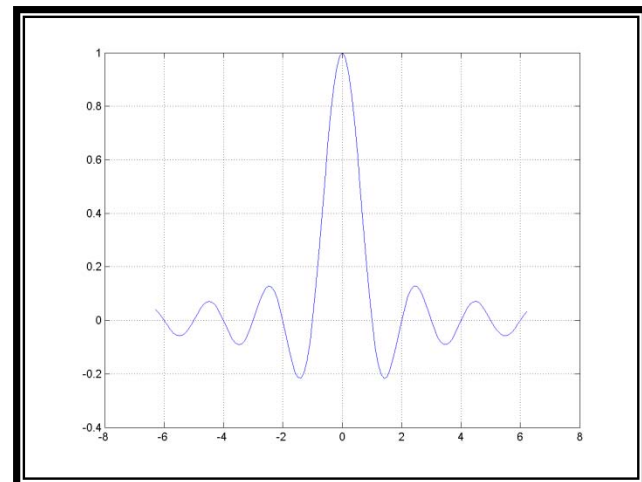
$$E_i = E_o e^{-j\frac{2\pi R_o}{\lambda}} e^{-j\frac{\pi d \sin(\theta)}{\lambda}} \left( e^{j\frac{\pi d \sin(\theta)}{\lambda}} + e^{-j\frac{\pi d \sin(\theta)}{\lambda}} \right)$$

$$E_i = 2E_o e^{-j\frac{2\pi R_o}{\lambda}} e^{-j\frac{\pi d \sin(\theta)}{\lambda}} \cos \frac{\pi d \sin(\theta)}{\lambda}$$

$$E_i \propto \sum_i E_{oi} \cos \left( \frac{2\pi d \sin(\theta)}{\lambda} \right)$$

If we increase from 0 to 90 degrees and reduce the resulting expression.

$$E_i \propto \frac{\sin x}{x}$$



# DC-8 and P-3B Antenna Configurations



MCoRDS, Accumulation, Snow, and Ku-band radars



# Example S/N ratio

See notes

|    |                           |             |       |         |         |       |
|----|---------------------------|-------------|-------|---------|---------|-------|
| 1  | Transmit power            | 500.00      | W     | 71.44   | dBm     |       |
| 2  | Transmit antenna gain     | 118.08      |       | 20.72   | dB      |       |
| 3  | Receive antenna gain      | 118.08      |       | 20.72   | dB      |       |
| 4  | Surface reflection loss   | 0.97        |       | -0.26   | dB      |       |
| 5  | Wavelength                | 1.54        |       | 3.74    |         |       |
| 6  | Bed reflection loss       | 0.10        |       | -20.00  | dB      |       |
| 7  | Ice loss                  | 20.00       | dB/km | 60.00   | dB      |       |
| 8  | Spreading loss            | 0.00        |       | -98.89  | dB      | dBm^2 |
| 9  | Received power            |             |       |         | -133.96 | dB    |
| 10 | Pulse compression gain    | 150.00      |       | 21.76   | dB      |       |
| 9  | Coherent integration gain | 1000        |       | 30.00   | dB      |       |
|    | Signal processing gain    |             |       |         | 51.76   |       |
| 10 | Boltzmann constant        | 0.00        |       | -228.60 |         |       |
| 11 | Temperature               | 290.00      | K     | 24.62   |         |       |
| 12 | Noise figure              | 2.00        |       | 3.01    |         |       |
| 13 | Bandwidth                 | 30000000.00 | Hz    | 74.77   |         |       |
| 14 | KTBF                      |             |       |         | -96.20  | dBm   |
|    | Signal-to-noise ratio     |             |       |         |         | 13.99 |

3/12/2012

$$\left(\frac{S}{N}\right)_M = \frac{P_T G_T G_r (1 - |\Gamma_{as}|^2) |\Gamma_b|^2 \lambda^2 C_g M}{(4\pi)^2 (2h)^2 L_s k T B F}$$

# Modern Radar

